## NUFAC 05 Institute Lectures

## Capri June 18/19 2005

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2 Lectures and Tutorial

1. preface (inc Solenoid Focus)
2. Transverse Ionization Cooling
3. Longitudinal Ionization Cooling
4. Tutorials

On data stick:
05schoolv2.pdf, icoolman.pdf, \& icool05.zip
On Web:
These Lectures and Tutorial
http://pubweb.bnl.gov/people/palmer/05school/05schoolv2.pdf
Files to Run problems with icool
http://pubweb.bnl.gov/people/palmer/05school/05icool.zip
Where to get generic icool files and manual
http://pubweb.bnl.gov/people/fernow/icool/readme.html
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## 1 PREFACE

### 1.1 Units

When discussing the motion of particles in magnetic fields, I will use MKS units, but this means that momentum, energy, and mass are in Joules and kilograms, rather than in the familiar 'electron Volts'. To make the conversion easy, I will introduce these quantities in the forms: $[p c / e],[E / e]$, and $\left[m c^{2} / e\right]$, respectively. Each of these expressions are then in units of straight Volts corresponding to the values of $p, E$ and $m$ expressed in electron Volts. For instance, I will write, for the bending radius in a field $B$ :

$$
\rho=\frac{[p c / e]}{B c}
$$

meaning that the radius for a $3 \mathrm{GeV} / \mathrm{c}$ particle in 5 Tesla is

$$
\rho=\frac{310^{9}}{5 \times 310^{8}}=2 m
$$

This units problem is often resolved in accelerator texts by expressing parameters in terms of $(B \rho)$ where this is a measure of momentum: the momentum that would have this value of $B \times \rho$, where

$$
(B \rho)=\frac{[p c / e]}{c}
$$

For $3 \mathrm{GeV} / \mathrm{c},(B \rho)$ is thus $10(\mathrm{Tm})$, and the radius of bending in a field $\mathrm{B}=5(\mathrm{~T})$ is:

$$
\rho=\frac{(B \rho)}{B}=\frac{10}{5}=2 m
$$

1.2 Useful Relativistic Relations

$$
\begin{align*}
d E & =\beta_{v} d p  \tag{1}\\
\frac{d E}{E} & =\beta_{v}^{2} \frac{d p}{p}  \tag{2}\\
d \beta_{v} & =\frac{d p}{\gamma^{2}} \tag{3}
\end{align*}
$$

I use $\beta_{v}$ to denote $v / c$ to distinguish it from the Courant-Schneider or Twiss parameters $\beta_{\perp}$

$$
\text { normalized emittance }=\frac{\text { Phase Space Area }}{\pi \mathrm{m} \mathrm{c}}
$$

The phase space can be transverse: $p_{x}$ vs $x, p_{y}$ vs $y$, or longitudinal $\Delta p_{z}$ vs $z$, where $\Delta p_{z}$ and $z$ are with respect to the moving bunch center.

If $x$ and $p_{x}$ are both Gaussian and uncorrelated, then the area is that of an upright ellipse, and:

$$
\begin{array}{cc}
\epsilon_{\perp}=\frac{\pi \sigma_{p_{\perp}} \sigma_{x}}{\pi m c}=\left(\gamma \beta_{v}\right) \sigma_{\theta} \sigma_{x} & (\pi m \mathrm{rad}) \\
\epsilon_{\|}=\frac{\pi \sigma_{p_{\|}} \sigma_{z}}{\pi m c}=\left(\gamma \beta_{v}\right) \frac{\sigma_{p}}{p} \sigma_{z} & (\pi \mathrm{mrad}) \\
\epsilon_{6}=\epsilon_{\perp}^{2} \epsilon_{\|} & (\pi m)^{3} \tag{6}
\end{array}
$$

Note that the $\pi$, added to the dimension, is a reminder that the emittance is phase space $/ \pi$
1.4 Beta $_{\perp}$ (Twiss) of Beam


Upright phase ellipse in $x^{\prime}$ vs $x$,

$$
\begin{equation*}
\beta_{\perp}=\left(\frac{\text { width }}{\text { height }} \quad \text { of phase ellipse }\right)=\frac{\sigma_{x}}{\sigma_{\theta}} \tag{7}
\end{equation*}
$$

Then, using emittance definition:

$$
\begin{gather*}
\sigma_{x}=\sqrt{\epsilon_{\perp} \beta_{\perp} \frac{1}{\beta_{v} \gamma}}  \tag{8}\\
\sigma_{\theta}=\sqrt{\frac{\epsilon_{\perp}}{\beta_{\perp}} \frac{1}{\beta_{v} \gamma}} \tag{9}
\end{gather*}
$$

1.4.1 $\operatorname{Beta}_{\perp}($ Twiss $)$ at focus

$\beta_{\perp}$ is like a depth of focus

As $z \rightarrow \infty$

$$
\sigma_{x} \rightarrow \frac{\sigma_{o} z}{\beta_{\perp}}
$$

giving an angular spread of

$$
\theta=\frac{\sigma_{o}}{\beta_{\perp}}
$$

as above in eq. 7
$\beta_{\perp}$ above was defined by the beam, but a lattice can have a $\beta_{\perp o}$ that may or may not "match" a beam.
e,g. if continuous inward focusing force, as in a current carrying lithium cylinder (lithium lens), then there is a PERIODIC solution:
$u$


$$
\frac{d^{2} u}{d z^{2}}=-k u \quad u=A \sin \left(\frac{z}{\beta_{\perp o}}\right) \quad u^{\prime}=\frac{A}{\beta_{o}} \cos \left(\frac{z}{\beta_{\perp o}}\right)
$$

where $k=c B /[p c / e] \quad \beta_{\perp o}=1 / \sqrt{k} \quad \lambda=2 \pi \beta_{o}$
This particle motion is also an ellipse and

$$
\frac{\text { width }}{\text { height }} \text { of elliptical motion in phase space }=\frac{\hat{u}}{\hat{u^{\prime}}}=\beta_{\perp o}
$$

If we have many particles with $\beta_{\perp}$ (Twiss) $=\beta_{\perp o}$ (Courant Snyder) then all particles move arround the ellipse, and the shape, and thus $\beta_{\perp}$ (Twiss) remains constant, and the beam is "matched" to this lattice.
If the beam's $\beta_{\perp}$ (Twiss) $\neq \beta_{\perp \text { o }}$ of the system then $\beta_{\perp}$ (Twiss of the beam oscillates about $\beta_{\perp_{o}}$ (Courant Snyder): often refered to as a "beta beat".
1.5 Introduction to Solenoid Focussing
1.5.1 Motion in Long Solenoid

Consider motion in a fixed axial filed $B_{z}$, starting on the axis O with finate transverse momentum $p_{\perp}$ i.e. with initial angular momentum $=0$.


For $\psi<180^{\circ} \quad \phi<90^{\circ}$ :

$$
\begin{gathered}
r=2 \rho \sin \left(\frac{\psi}{2}\right)=2 \rho \sin (\phi) \\
\frac{d z}{d \phi}=2 \rho \frac{p_{z}}{p_{\perp}}
\end{gathered}
$$

### 1.5.2 Larmor Plane

If The center of the solenoid magnet is at $O$, then consider a plane that contains this axis and the particle. This, for a particle with initally no angular momentum, is the 'Larmor Plane:


$$
\begin{align*}
u & =2 \rho \sin (\phi)  \tag{11}\\
\lambda_{\text {Helix }}=2 \pi \frac{d z}{d \psi} & =2 \pi \rho \frac{p_{z}}{p_{\perp}}=2 \pi \frac{[p c / e]_{z}}{c B_{z}} \\
\lambda_{\text {Larmor }}=2 \pi \frac{d z}{d \phi} & =2 \pi 2 \rho \frac{p_{z}}{p_{\perp}}=4 \pi \frac{[p c / e]_{z}}{c B_{z}}
\end{align*}
$$

The lattice parameter $\beta_{o}$ is defined in the Larmor frame, so

$$
\begin{equation*}
\beta_{o}=\frac{\lambda_{\text {Larmor }}}{2 \pi}=\frac{2[p c / e]_{z}}{c B_{z}} \tag{12}
\end{equation*}
$$

In this constant $B$ case, the observed sinusoidal motion in the $u$ plane is generated by a restoring force towards the axis 0 .
The momentum $p_{O}$ about the axis O (perpendicular to the Larmor plane), using eq. 10 and eq.11:

$$
\begin{equation*}
\left[p_{O} c / e\right]=\left[p_{\perp} c / e\right] \sin (\phi)=c B_{z} \rho \frac{u}{2 \rho}=\frac{c B_{z}}{2} u \tag{13}
\end{equation*}
$$

And the inward bending as this momentum crosses the $B_{z}$ field is

$$
\begin{equation*}
\frac{d^{2} u}{d z^{2}}=-\left(\frac{c B_{z}}{2\left[p_{z} c / e\right]}\right)^{2} u \tag{14}
\end{equation*}
$$

This inward force proportional to the distance $u$ from the axis is an ideal focusing force
Note: the focusing "Force" $\propto B_{z}^{2}$ so it works the same for either sign, and $\propto 1 / p_{z}^{2}$. Whereas in a quadrupole the force $\propto 1 / p$ So solenoids are not good for high $p$, but beat quads at low $p$.

### 1.5.4 Entering a solenoid from outside

We will now look at a simple non-uniform $B_{z}$ case. Let a particle start from the axis with finite transverse momentum, but no angular momentum. After some distance with no field, it reaches a radius $u$ and then enters a solenoid with $B_{z}$. As it enters the solenoid it crosses radial field lines and receives some angular momentum.


$$
\begin{equation*}
\Delta[p c / e]_{\perp}=\int B_{r} d z=\frac{B_{z} r c}{2} \tag{15}
\end{equation*}
$$

Sof for our case with zero initial transverse momentum,

$$
[p c / e]_{\perp}=\int B_{r} d z=\frac{B_{z} r c}{2}
$$

Which is the same as eq.13, and will lead to the same inward bending (eq.14), as when the particle started inside the field.

In fact eq. 14 is true no matter how the axial field varies

### 1.5.5 Canonical Angular momentum

In general, for axial symmetry, a particle will have a conserved "Canonical Angular Momentum" $\mathcal{M}_{o}$ equal to the angular momentum outside the axial fields.

$$
\left[\mathcal{M} c^{2} / e\right]_{o}=p_{\perp} r(\text { Outdise the field })
$$

Inside a varying field $B_{z}(z)$, the real angular momentum will be:

$$
\left[\mathcal{M} c^{2} / e\right]=\left[\mathcal{M} c^{2} / e\right]_{o}+\frac{r^{2} B_{z} c}{2}
$$

But in the rotating Larmor Frame the angular momentum is always just the Canonical angular momentum, and motion in that frame has only inward focusing forces, with no angular kicks.

## 2 TRANSVERSE IONIZATION COOLING


2.1 Cooling rate vs. Energy

$$
(\mathrm{eq} 4) \quad \epsilon_{x, y}=\gamma \beta_{v} \sigma_{\theta} \sigma_{x, y}
$$

If there is no Coulomb scattering, or other sources of emittance heating, then $\sigma_{\theta}$ and $\sigma_{x, y}$ are unchanged by energy loss, but $p$ and thus $\beta \gamma$ are reduced. So the fractional cooling $d \epsilon / \epsilon$ is (using eq.2):

$$
\begin{equation*}
\frac{d \epsilon}{\epsilon}=\frac{d p}{p}=\frac{d E}{E} \frac{1}{\beta_{v}^{2}} \tag{16}
\end{equation*}
$$

which, for a given energy change, strongly favors cooling at low energy.

But if total acceleration were not important, e.g. if the cooling is done in a ring, then there is another criterion: The cooling per fractional loss of particles by decay:

$$
\begin{aligned}
Q= & \frac{d \epsilon / \epsilon}{d n / n}=\frac{d p / p}{d \ell / c \beta_{v} \gamma \tau} \\
& =\frac{d E / E 1 / \beta_{v}^{2}}{d \ell /\left(c \gamma \beta_{v} \tau\right)} \\
= & \left(c \tau / m_{\mu}\right) \frac{d E}{d \ell} \frac{1}{\beta_{v}}
\end{aligned}
$$

Which only mildly favours low energy

### 2.2 Heating Terms

$$
\epsilon_{x, y}=\gamma \beta_{v} \sigma_{\theta} \sigma_{x, y}
$$

Between scatters the drift conserves emittance (Liouiville).
When there is scattering, $\sigma_{x, y}$ is conserved, but $\sigma_{\theta}$ is increased.

$$
\begin{gathered}
\Delta\left(\epsilon_{x, y}\right)^{2}=\gamma^{2} \beta_{v}^{2} \sigma_{x, y}^{2} \Delta\left(\sigma_{\theta}^{2}\right) \\
2 \epsilon \Delta \epsilon=\gamma^{2} \beta_{v}^{2}\left(\frac{\epsilon \beta_{\perp}}{\gamma \beta_{v}}\right) \Delta\left(\sigma_{\theta}^{2}\right) \\
\Delta \epsilon=\frac{\beta_{\perp} \gamma \beta_{v}}{2} \Delta\left(\sigma_{\theta}^{2}\right)
\end{gathered}
$$

e.g. from Particle data booklet

$$
\begin{gathered}
\Delta\left(\sigma_{\theta}^{2}\right) \approx\left(\frac{14.110^{6}}{[p c / e] \beta_{v}}\right)^{2} \frac{\Delta s}{L_{R}} \\
\Delta \epsilon=\frac{\beta_{\perp}}{\gamma \beta_{v}^{3}} \Delta E\left(\left(\frac{14.110^{6}}{2\left[m c^{2} / e\right]_{\mu}}\right)^{2} \frac{1}{L_{R} d E / d s}\right)
\end{gathered}
$$

Defining

$$
\begin{equation*}
C(m a t, E)=\frac{1}{2}\left(\frac{14.110^{6}}{\left.\left[m c^{2} / e\right]_{\mu}\right)}\right)^{2} \frac{1}{L_{R} d \gamma / d s} \tag{17}
\end{equation*}
$$

then

$$
\begin{equation*}
\frac{\Delta \epsilon}{\epsilon}=d E \frac{\beta_{\perp}}{\epsilon \gamma \beta_{v}^{3}} C(\text { mat }, E) \tag{18}
\end{equation*}
$$

Equating this with equation 16

$$
d E \frac{1}{\beta_{v}^{2} E}=d E \frac{\beta_{\perp}}{\epsilon \gamma \beta_{v}^{3}} C(\text { mat, } E)
$$

gives the equilibrium emittance $\epsilon_{o}$ :

$$
\begin{equation*}
\epsilon_{x, y}(\min )=\frac{\beta_{\perp}}{\beta_{v}} C(\text { mat }, E) \tag{19}
\end{equation*}
$$

At energies such as to give minimum ionization loss, the constant $C_{o}$ for various materials are approximately:

| material | T <br> ${ }^{o} \mathrm{~K}$ | density <br> $\mathrm{kg} / \mathrm{m}^{3}$ | $\mathrm{dE} / \mathrm{dx}$ <br> $\mathrm{MeV} / \mathrm{m}$ | $L_{R}$ <br> m | $C_{o}$ <br> $10^{-4}$ |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Liquid $\mathrm{H}_{2}$ | 20 | 71 | 28.7 | 8.65 | 38 |
| Liquid He | 4 | 125 | 24.2 | 7.55 | 51 |
| LiH | 300 | 820 | 159 | 0.971 | 61 |
| Li | 300 | 530 | 87.5 | 1.55 | 69 |
| Be | 300 | 1850 | 295 | 0.353 | 89 |
| Al | 300 | 2700 | 436 | 0.089 | 248 |



Clearly Liquid Hydrogen is far the best material, but has cryogenic and safety complications, and requires windows made of Aluminum or other material which will significantly degrade the performance.
2.3 Rate of Cooling

$$
\begin{equation*}
\frac{d \epsilon}{\epsilon}=\left(1-\frac{\epsilon_{\min }}{\epsilon}\right) \frac{d p}{p} \tag{20}
\end{equation*}
$$

$$
\sigma_{\theta}=\sqrt{\frac{\epsilon_{\perp}}{\beta_{\perp} \beta_{v} \gamma}}
$$

so, from equation 19, for a beam in equilibrium

$$
\sigma_{\theta}=\sqrt{\frac{C(m a t, E)}{\beta_{v}^{2} \gamma}}
$$

and for $50 \%$ of maximum cooling rate and an aperture at $3 \sigma$, the angular aperture $\mathcal{A}$ of the system must be

$$
\begin{equation*}
\mathcal{A}=3 \sqrt{2} \sqrt{\frac{C(m a t, E)}{\beta_{v}^{2} \gamma}} \tag{21}
\end{equation*}
$$

Apertures for hydrogen and lithium are plotted vs. energy below. These are very large angles, and if we limit apertures to less than 0.3 , then this requirement sets lower energy limits of about $100 \mathrm{MeV}(\approx 170 \mathrm{MeV} / \mathrm{c})$ for Lithium, and about $25 \mathrm{MeV}(\approx 75 \mathrm{MeV} / \mathrm{c})$ for hydrogen.
$\theta=0.3$ may be about as large as is possible in a lattice, but larger angles may be sustainable in a continuous focusing system such as a lens or solenoid. is optimistic, as we will see in the tutorial.


### 2.5 Focusing Systems

### 2.5.1 Solenoid

In a solenoid with axial field $B_{\text {sol }}$ (from eq 12)

$$
\beta_{\perp}=\frac{2[p c / e]}{c B_{s o l}}
$$

so

$$
\begin{equation*}
\epsilon_{x, y}(\min )=C(m a t, E) \frac{2 \gamma\left[m c^{2} / e\right]_{\mu}}{B_{\text {sol }} c} \tag{22}
\end{equation*}
$$

For $E=100 \mathrm{MeV}(p \approx 170 \mathrm{MeV} / \mathrm{c}), B=10 \mathrm{~T}$, then $\beta \approx 11.4 \mathrm{~cm}$. and $\epsilon_{x, y}(\min ) \approx 532(\pi \mathrm{~mm} \operatorname{mrad})$.

### 2.5.2 Current Carrying Rod

In a rod carrying a uniform axial current, the azimuthal magnetic field $B$ varies linearly with the radius $r$. A muon traveling down it is focused:

$$
\frac{d^{2} r}{d r^{2}}=-\frac{B c}{[p c / e]}=-\left(\frac{c}{[p c / e]} \frac{d B}{d r}\right) r
$$

so orbits oscillate with

$$
\begin{equation*}
\beta_{\perp}^{2}=\frac{\gamma \beta_{v}}{d B / d r} \frac{\left[m c^{2} / e\right]_{\mu}}{c} \tag{23}
\end{equation*}
$$

If we set the rod radius $a$ to be $f_{a p}$ times the rms beam size $\sigma_{x, y}$ (from eq.8),

$$
\sigma_{x, y}=\sqrt{\frac{\epsilon_{x, y} \beta_{\perp}}{\beta_{v} \gamma}}
$$

and if the field at the surface is $B_{\max }$, then

$$
\beta_{\perp}^{2}=\frac{\gamma \beta_{v}\left[m c^{2} / e\right]_{\mu} f_{a p}}{B_{\max } c} \sqrt{\frac{\epsilon_{x, y} \beta}{\gamma \beta_{v}}}
$$

from which we get:

$$
\beta_{\perp}=\left(\frac{f_{a p}\left[m c^{2} / e\right]_{\mu}}{B_{\max } c}\right)^{2 / 3}\left(\gamma \beta_{v} \epsilon_{x, y}\right)^{1 / 3}
$$

puting this in equation 19

$$
\begin{equation*}
\epsilon_{x, y}(\min )=(C(\text { mat }, E))^{1.5}\left(\frac{f_{a p}\left[m c^{2} / e\right]_{\mu}}{B_{\max } c \beta_{v}}\right) \sqrt{\gamma} \tag{24}
\end{equation*}
$$

e.g. $B_{\max }=10 \mathrm{~T}, f_{a p}=3, \mathrm{E}=100 \mathrm{MeV}$, then $\beta_{\perp}=1.23 \mathrm{~cm}$, and
$\epsilon_{x, y}($ min $)=100 \quad(\pi \mathrm{~mm} \mathrm{mrad})$
The choice of a maximum surface field of 10 T is set by breaking of the containing pipe in current solid Li designs. With liquid Li a higher field may be possible.

### 2.5.3 Compare Focusing

Comparing the methods as a function of the beam kinetic energy.


We see that, for the parameters selected, The lithium rod achieves a lower emittance than the solenoid despite its higher $C$ value. Neither method allows transverse cooling below about 80 ( $\pi \mathrm{mm} \mathrm{mrad}$ ), except at very low energies.

### 2.6 Li Lens to meet 3 TeV Collider Final Emittance

At lower energies the minimum emittance is lower and can meet the 50 pi mm mrad requirement for a 5 TeV collider. But the $\mathrm{dp} / \mathrm{p}$ rises rapidly because of the reverse slope of $\mathrm{dE} / \mathrm{dx}$. Never the less, the 6D emittance does not rise. The effect is that of an emittance exchange between longitudinal and transverse emittances.



- Work needed on Matching in and out
2.7 Decreasing beta in Solenoids by adding periodicity

Parametric-Resonance Ionization Cooling (PIC) (Derbenev ${ }^{1}$ ) / FOFO (Palmer)



- Determination of lattice betas
- Track single near paraxial particle through many cells
- plot $\theta_{x}$ vs x after each cell
- fit ellipse: $\beta_{x, y}=\mathrm{A}\left((\mathrm{x}) / \mathrm{A}\left(\theta_{x}\right)\right.$
- Resonances introduced
- Betas reduced locally
- Momentum acceptance small

[^0]
## Super FOFO

Double periodicity



- Beta lower over finite momentum range
- Beta lower by about $1 / 2$ solenoid


### 2.8 Angular Momentum Problem in Solenoid Cases

In the absence of external fields and energy loss in materials, the angular momentum of a particle is conserved.

But a particle entering a solenoidal field will cross radial field components and its angular momentum ( $r p_{\phi}$ ) will change (eq.15).

$$
r \Delta\left([p c / e]_{\phi}\right)=r \Delta\left(\frac{c B_{z} r}{2}\right)
$$

If, in the absence of the field, the particle had "canonical" angular momentum $\left(p_{\phi} r\right)_{\text {can }}$, then in the field it will have angular momentum:

$$
[p c / e]_{\phi} r=\left(p_{\phi} r\right)_{\mathrm{can}}+\left(\frac{c B_{z} r}{2}\right) r
$$

SO

$$
\begin{equation*}
\left.[p c / e]_{\phi} r\right)_{\mathrm{can}}=[p c / e]_{\phi} r-\left(\frac{c B_{z} r}{2}\right) r \tag{25}
\end{equation*}
$$

If the initial average canonical angular momentum is zero, then in $B_{z}$ :

$$
<[p c / e]_{\phi} r>=\left(\frac{c B_{z} r}{2}\right) r
$$

Material introduced to cool the beam, will reduce all momenta, both longitudinal and transverse, random and average.

Re-acceleration will not change the angular momenta, so the average angular momentum will continuously fall.

Consider the case of almost complete transverse cooling: all transverse momenta are reduced to near zero leaving the beam streaming parallel to the axis.

$$
[p c / e]_{\phi} r \approx 0
$$

and there is now a finite average canonical momentum (from eq.25):

$$
<[p c / e]_{\phi} r>_{\mathrm{can}}=-\left(\frac{c B_{z} r}{2}\right) r
$$

When the beam exits the solenoid, then this canonical angular momentum becomes a real angular momentum and represents an effective emittance, and severely limits the possible cooling.

$$
<[p c / e]_{\phi} r>_{\text {end }}=-\left(\frac{c B_{z} r}{2}\right) r
$$

The only reasonable solution is to reverse the field, either once, a few, or many times.

The minimum required number of field "flips" is one.


After exiting the first solenoid, we have real coherent angular momentum:

$$
\left([p c / e]_{\phi} r\right)_{3}=-\left(\frac{c B_{z 1} r}{2}\right) r
$$

The beam now enters a solenoid with opposite field $B_{z 2}=-B_{z 1}$.
The canonical angular momentum remains the same, but the real angular momentum is dou-
bled.

$$
\left([p c / e]_{\phi} r\right)_{4}=-2\left(\frac{c B_{z 1} r}{2}\right) r
$$

We now introduce enough material to halve the transverse field components. Then

$$
\left([p c / e]_{\phi} r\right)_{5}=-\left(\frac{c B_{z 1} r}{2}\right) r
$$

This is inside the field $B_{z 2}=-B_{z 1}$. The canonical momentum, and thus the angular momentum on exiting, is now:

$$
\left([p c / e]_{\phi} r\right)_{6}=-\left(\frac{c B_{z 1} r}{2}\right) r--\left(\frac{c B_{z 1} r}{2}\right) r=0
$$

2.9 Examples of Focus Design

### 2.9.1 Continuous Solenoid

Coils Outside RF: e.g. FNAL 1 flip

"Flip" Design
One must design the flips to match the betas from one side to the other.

For a computer designed matched flip between uniform solenoidal fields: the following figure shows $B_{z}$ vs. $z$ and the $\beta_{\perp}$ 's vs. $z$ for different momenta.


2.9.2 Lattices with many "flips"


# SFOFO Lattice Engineering <br> Study 2 at Start of Cooling 



- This is the lattice to be tested in Muon lonization Cooling Experiemnt (MICE) at RAL
- In study 2 the lattice is modified vs. length to lower $\beta_{\perp}$ as $\epsilon$ falls

This keeps $\sigma_{\theta}$ and $\epsilon / \epsilon_{o}$ more or less constant, thus maintains cooling rate

## Study 2 Performance



With RF and Hydrogen Windows, $C_{o} \approx 4510^{-4}$
$\beta_{\perp}($ end $)=.18 \mathrm{~m}, \quad \beta_{v}($ end $)=0.85$, So

$$
\begin{gathered}
\epsilon_{\perp}(\min )=\frac{4510^{-4} 0.18}{0.85}=0.95(\pi \mathrm{~mm} \mathrm{mrad}) \\
\frac{\epsilon_{\perp}}{\epsilon_{\perp}(\min )}
\end{gathered}
$$

so from eq. 20

$$
\frac{d \epsilon}{\epsilon}(\mathrm{end})=\left(1-\frac{\epsilon}{\epsilon(\min )}\right) \frac{d p}{p} \approx 0.57 \frac{d p}{p}
$$

## 3 LONGITUDINAL IONIZATION COOLING

Following the convention for synchrotron cooling we define partition functions:

$$
\begin{align*}
& J_{x, y, z}=\frac{\frac{\Delta\left(\epsilon_{x, y, z}\right)}{\epsilon_{x, y, z}}}{\frac{\Delta p}{p}}  \tag{26}\\
& J_{6}=J_{x}+J_{y}+J_{z} \tag{27}
\end{align*}
$$

where the $\Delta \epsilon$ 's are those induced directly by the energy loss mechanism (ionization energy loss in this case). $\Delta p$ and $p$ refer to the loss of momentum induced by this energy loss.

In electron synchrotrons, with no gradients fields, $J_{x}=J_{y}=1$, and $J_{z}=2$.
In muon ionization cooling, $J_{x}=J_{y}=1$, but $J_{z}$ is negative or small.

## 3.1 c.f. Transverse

From last lecture:

$$
\frac{\Delta \sigma_{p \perp}}{\sigma_{p \perp}}=\frac{\Delta p}{p}
$$

and $\sigma_{x, y}$ does not change, so

$$
\begin{equation*}
\frac{\Delta \epsilon_{x, y}}{\epsilon_{x, y}}=\frac{\Delta p}{p} \tag{28}
\end{equation*}
$$

and thus

$$
\begin{equation*}
J_{x}=J_{y}=1 \tag{29}
\end{equation*}
$$

3.2 Longitudinal cooling/heating without wedges


The emittance in the longitudinal direction $\epsilon_{z}$ is (eq.5):

$$
\epsilon_{z}=\gamma \beta_{v} \frac{\sigma_{p}}{p} \sigma_{z}=\frac{1}{m} \sigma_{p} \sigma_{z}=\frac{1}{m} \sigma_{E} \sigma_{t}=c \sigma_{\gamma} \sigma_{t}
$$

where $\sigma_{t}$ is the rms bunch length in time, and $c$ is the velocity of light. Drifting between interactions will not change emittance (Louville), and an interaction will not change $\sigma_{t}$, so emittance change is only induced by the energy change in the interactions:

$$
\frac{\Delta \epsilon_{z}}{\epsilon_{z}}=\frac{\Delta \sigma_{\gamma}}{\sigma_{\gamma}}=\frac{\sigma_{\gamma} \Delta s \frac{d(d \gamma / d s)}{d \gamma}}{\sigma_{\gamma}}=\Delta s \frac{d(d \gamma / d s)}{d \gamma}
$$

and

$$
\frac{\Delta p}{p}=\frac{\Delta \gamma}{\beta_{v}^{2} \gamma}=\frac{\ell}{\beta_{v}^{2} \gamma}\left(\frac{d \gamma}{d s}\right)
$$

So from the definition of the partition function $J_{z}$ :

$$
\begin{equation*}
J_{z}=\frac{\frac{\Delta \epsilon_{z}}{\epsilon_{z}}}{\frac{\Delta p}{p}}=\frac{\left(\Delta s \frac{d(d \gamma / d s)}{d \gamma}\right)}{\frac{\Delta s}{\beta_{v}^{2} \gamma}\left(\frac{d \gamma}{d s}\right)}=\frac{\left(\beta_{v}^{2} \frac{d(d \gamma / d s)}{d \gamma / \gamma}\right)}{\left(\frac{d \gamma}{d s}\right)} \tag{30}
\end{equation*}
$$

A typical relative energy loss as a function of energy is shown above (this example is for Lithium). It is given approximately by:


$$
\begin{equation*}
\frac{d \gamma}{d s}=B \frac{1}{\beta_{v}^{2}}\left(\frac{1}{2} \ln \left(A \beta_{v}^{4} \gamma^{4}-\beta_{v}^{2}\right)\right. \tag{31}
\end{equation*}
$$

where

$$
\begin{equation*}
A=\frac{\left(2 m_{e} c^{2} / e\right)^{2}}{I^{2}} \quad B \approx \frac{0.0307}{\left(m_{\mu} c^{2} / e\right)} \frac{Z}{A} \tag{32}
\end{equation*}
$$

where $Z$ and $A$ are for the nucleus of the material, and $I$ is the ionization potential for that material.
Differentiating the above:

$$
\frac{\delta(d \gamma / d s)}{\delta \gamma}=\frac{B}{\beta_{v}}\left(\frac{2}{\beta_{v} \gamma}-\frac{1}{\left(\beta_{v} \gamma\right)^{3}} \ln \left(A \beta_{v}^{4} \gamma^{4}\right)+\frac{2}{\left(\beta_{v} \gamma\right)^{3}}\right)
$$

Substituting this into equation 30 :

$$
\begin{equation*}
J_{z}(\text { no wedge }) \approx-\frac{\left(\frac{2}{\beta_{v} \gamma}-\frac{1}{\left(\beta_{v} \gamma\right)^{3}} \ln \left(A \beta_{v}^{4} \gamma^{4}\right)+\frac{2}{\left(\beta_{v} \gamma\right)^{3}}\right)}{\left(\frac{1}{2} \ln \left(A \beta_{v}^{4} \gamma^{4}-\beta_{v}^{2}\right)\right.} \beta_{v}^{3} \gamma \tag{33}
\end{equation*}
$$

It is seen that $J_{z}$ is strongly negative at low energies (longitudinal heating), and is only barely positive at momenta above $300 \mathrm{MeV} / \mathrm{c}$. In practice there are many reasons to cool at a moderate momentum around $250 \mathrm{MeV} / \mathrm{c}$, where $J_{z} \approx 0$. However, the 6D cooling is still strong $J_{6} \approx 2$.


What is needed is a method to exchange cooling between the transverse and longitudinal direction s . This is done in synchrotron cooling if focusing and bending is combined, but in this case, and in general, one can show that such mixing can only increase one $J$ at the expense of the others: $J_{6}$ is conserved.

$$
\begin{equation*}
\Delta J_{x}+\Delta J_{x}+\Delta J_{x}=0 \tag{34}
\end{equation*}
$$

and for typical operating momenta:

$$
\begin{equation*}
J_{x}+J_{y}+J_{z}=J_{6} \approx 2.0 \tag{35}
\end{equation*}
$$


3.4 Longitudinal cooling withy wedges and Dispersion



For a wedge with center thickness $\ell$ and height from center $h(2 h \tan (\theta / 2)=\ell)$, in dispersion $D\left(D=\frac{d y}{d p / p}\right.$, or with eq.2: $\left.D=\beta_{v}^{2} \frac{d y}{d \gamma / \gamma}\right)$ (see fig. above):

$$
\frac{\Delta \epsilon_{z}}{\epsilon_{z}}=\frac{\Delta \sigma_{\gamma}}{\sigma_{\gamma}}=\frac{\sigma_{\gamma} \frac{d s}{d \gamma}\left(\frac{d \gamma}{d s}\right)}{\sigma_{\gamma}}=\frac{d s}{d \gamma}\left(\frac{d \gamma}{d s}\right)=\left(\frac{\ell}{h}\right) \frac{D}{\beta_{v}^{2} \gamma}\left(\frac{d \gamma}{d s}\right)
$$

and

$$
\frac{\Delta p}{p}=\frac{\Delta \gamma}{\beta_{v}^{2} \gamma}=\frac{\ell}{\beta_{v}^{2} \gamma}\left(\frac{d \gamma}{d s}\right)
$$

So from the definition of the partition function $J_{z}$ :

$$
\begin{gather*}
\Delta J_{z}(\text { wedge })=\frac{\frac{\Delta \epsilon_{z}}{\epsilon_{z}}}{\frac{\Delta p}{p}}=\frac{\left(\frac{\ell}{h}\right) \frac{D}{\beta_{v}^{2} \gamma}\left(\frac{d \gamma}{d s}\right)}{\frac{\ell}{\beta_{v}^{2} \gamma}\left(\frac{d \gamma}{d s}\right)}=\frac{D}{h} \quad\left(\text { for simple bend \& gas } \Delta J_{z}(\text { wedge })=1\right)  \tag{36}\\
J_{z}=J_{z}(\text { no wedge })+\Delta J_{z}(\text { wedge }) \tag{37}
\end{gather*}
$$

But from eq.34, for any finite $J_{z}$ (wedge), $J_{x}$ or $J_{y}$ will change in the opposite direction.

### 3.5 Longitudinal Heating Terms

Since $\epsilon_{z}=\sigma_{\gamma} \sigma_{t} c$, and $t$ and thus $\sigma_{t}$ is conserved in an interaction

$$
\frac{\Delta \epsilon_{z}}{\epsilon_{z}}=\frac{\Delta \sigma_{\gamma}}{\sigma_{\gamma}}
$$

Straggling, from Perkins text book, converted to MKS:

$$
\Delta\left(\sigma_{\gamma}\right)=\frac{\Delta \sigma_{\gamma}^{2}}{2 \sigma_{\gamma}} \approx \frac{1}{2 \sigma_{\gamma}} 0.06 \frac{Z}{A}\left(\frac{m_{e}}{m_{\mu}}\right)^{2} \gamma^{2}\left(1-\frac{\beta_{v}^{2}}{2}\right) \rho \Delta s
$$

From eq. 2: $\Delta E=E \beta_{v}^{2} \frac{\Delta p}{p}$, so:

$$
\Delta s=\frac{\Delta E}{d E / d s}=\frac{1}{d E / d s} E \beta_{v}^{2} \frac{\Delta p}{p}
$$

so

$$
\frac{\Delta \epsilon_{z}}{\epsilon_{z}}=\frac{0.06}{2 \sigma_{\gamma}^{2}} \frac{Z}{A}\left(\frac{m_{e}}{m_{\mu}}\right)^{2} \gamma^{2}\left(1-\frac{\beta_{v}^{2}}{2}\right) \rho \frac{\beta_{v}^{2} E}{d E / d s} \frac{\Delta p}{p}
$$

This can be compared with the cooling term

$$
\frac{\Delta \epsilon_{z}}{\epsilon_{z}}=-J_{z} \frac{d p}{p}
$$

giving an equilibrium:

$$
\begin{equation*}
\frac{\sigma_{p}}{p}=\left(\left(\frac{m_{e}}{m_{\mu}}\right) \sqrt{\frac{0.06 Z \rho}{2 A(d \gamma / d s)}}\right) \sqrt{\frac{\gamma}{\beta_{v}^{2}}\left(1-\frac{\beta_{v}^{2}}{2}\right) \frac{1}{J_{z}}} \tag{38}
\end{equation*}
$$

For Hydrogen, the value of the first parenthesis is $\approx 1.36 \%$.

Without coupling, $J_{z}$ is small or negative, and the equilibrium does not exist. But with equal partition functions giving $J_{z} \approx 2 / 3$ then this expression, for hydrogen, gives: the values plotted below.
The following plot shows the dependency for hydrogen


It is seen to favor cooling at around $200 \mathrm{MeV} / \mathrm{c}$, but has a broad minimum.

### 3.5.1 rf and bunch length

To obtain the Longitudinal emittance we need $\sigma_{z}$.
If the rf acceleration is relatively uniform along the lattice, then we can write the synchrotron wavelength ${ }^{2}$ :

$$
\begin{equation*}
\lambda_{s}=\sqrt{\frac{\left.2 \pi \beta_{v}^{2} \lambda_{r f} \gamma\left[m c^{2} / e\right]_{\mu}\right)}{\mathcal{E}_{\mathrm{rf}} \alpha \cos (\phi)}} \tag{39}
\end{equation*}
$$

where, in a linear lattice, the "momentum compaction" is:

$$
\begin{equation*}
\alpha=\frac{\frac{d v_{z}}{v_{z}}}{\frac{d p}{p}}=\frac{1}{\gamma^{2}} \tag{40}
\end{equation*}
$$

and the field $\mathcal{E}_{\mathrm{rf}}$ is the rf accelerating field; $\phi$ is the rf phase, defined so that for $\phi=0$ there is zero acceleration.
The bunch length, given the relative momentum spread $d p / p=\delta$, is given by ${ }^{3}$ :

$$
\begin{equation*}
\sigma_{z}=\delta \beta_{v} \frac{\alpha \lambda_{s}}{2 \pi}=\delta \beta_{v}^{2} \sqrt{\frac{\lambda_{r f}\left[m c^{2} / e\right]_{\mu}}{2 \pi \gamma \mathcal{E} \cos (\phi)}} \tag{41}
\end{equation*}
$$

This, in the following plot, is seen to be only weakly dependent on the energy, but the longitudinal emittance $\epsilon_{z}=\beta_{v} \gamma \sigma p / p \sigma_{z}$ rises almost linearly with momentum, strongly favoring low momenta.
It is also apparent that the emittance can be reduced if a higher frequency and higher gradient rf is used. The limit her is when the ratio of $\sigma_{z} / \lambda$ becomes too large and particles do not remain in the bucket.

[^1]3.6 Emittance Exchange Studies

- Wedges in Bent Solenoids

Problem with rf due to slip

- Ring with with solenoid focus (Balbakov ${ }^{4}$ ) achieved Merit=90 but not real fields
- Quadrupole focused ring (Garren et al ${ }^{5}$ )
achieved Merit $\approx 15$, no end fields
- Ring with Maxwellian Bend only focusing (Garren et al) achieved Merit 10-100
- RFOFO Ring (Palmer et al ${ }^{6}$ )
achieved Merit $\approx 140$ with real fields
- Wedges in with Maxwellian Helical fields ${ }^{7}$

Good performance, but fields very high if coils outside rf

[^2]

- Gas used partly for higher gradients Not yet demonstrated
- $J_{z}<1$ can be set to $2 / 3$
- Cooling in 6 dimensions
of order 1000
- Moderate fields at beam
$\mathrm{Bz}=3.5 \mathrm{~T} . \mathrm{Br}=.5 \mathrm{~T}$
- Better Performance than RFOFO Ring


[^3]
## But Helix Fields at Coils > 24 T



- Increasing pitch: hurts $\mathrm{ds} / \mathrm{dp}$
- Decreasing helix B: hurts $\mathrm{ds} / \mathrm{dp}$
- Lowering RF $\lambda \rightarrow$ lower emit + higher B's
- Exploring emittance exchange before bunching and RF


### 3.8 Example 2) RFOFO Ring

## R.B. Palmer R. Fernow J. Gallardo ${ }^{9}$, and Balbekov ${ }^{10}$



[^4]
## Performance

Using Real Fields, but no windows or injection insertion

$$
\text { Merit }=\frac{n}{n_{o}} \frac{\epsilon_{6, o}}{\epsilon_{6}}=\frac{\text { Initial phase density }}{\text { final phase density }}
$$


3.8.1 Compare Simulation with theory
$D=7 \mathrm{~cm}, \ell=28.6 \mathrm{~cm}$, and

$$
\begin{gathered}
h=\frac{\ell}{2 \tan \left(100^{\circ} / 2\right)}=12 \mathrm{~cm} \\
J_{z}=\frac{D}{h}=0.58
\end{gathered}
$$

Since there is good mixing between $x$ and $y$ so $J_{x}=J_{y}$, and from equ $35, \Sigma J_{i} \approx 2.0$, so

$$
J_{x}=J_{y} \approx \frac{2-0.58}{2}=0.71
$$

i.e. The wedge angle gave nearly equal partition functions in all 3 coordinates, and gives the maximum merit factor.
The theoretical equilibrium emittances are now (eq.19):

$$
\epsilon_{\perp}(\min )=\frac{C \beta_{\perp}}{J \beta_{v}}=\frac{3810^{-4} 0.4}{0.710 .85}=2.5(\pi \mathrm{~mm})
$$

c.f. $2.43(\pi \mathrm{~mm})$ observed, which is very good agreement considering the approximations used.

And from equation 38 we expect

$$
\frac{d p}{p}(\min ) \approx 2.3 \%
$$

compared with $3.6 \%$ observed, which is less good agreement. This may arise from the poorer approximation of the real Landau scattering distribution by a simple Gaussian.
3.8.2 Insertion for Injection/Extraction


- Merit Factor $139 \rightarrow 100$


## Minimum Required kick



$$
f_{\sigma}=\frac{\mathrm{Ap}}{\sigma} \quad \mu(\text { of return })=\inf \quad F=\frac{Y}{X}
$$



$$
\begin{gathered}
I=F\left(\frac{4 f_{\sigma}^{2}\left[m_{\mu} c^{2} / e\right]}{\mu_{o} c}\right) \frac{\epsilon_{n}}{L} \\
V=\left(\frac{4 f_{\sigma}^{2}\left[m_{\mu} c^{2} / e\right] R}{c}\right) \frac{\epsilon_{n}}{\tau} \\
U=F\left(\frac{\left[m_{\mu} c^{2} / e\right]^{2} 8 f_{\sigma}^{4} R}{\mu_{o} c^{2}}\right) \frac{\epsilon_{n}^{2}}{L}
\end{gathered}
$$

- muon $\epsilon_{n} \gg$ other $\epsilon_{n}$ 's
- So muon kicker Joules $\gg$ other kickers
- Nearest are $\bar{p}$ kickers

Compare with others
For $\epsilon_{\perp}=10 \pi \mathrm{~mm}$, (Acceptance $=90$ pi mm) $\quad \beta_{\perp}=1 \mathrm{~m}, \& \tau=50 \mathrm{nsec}:$
After correction for finite $\mu$ and leakage flux:

|  |  | $\mu$ Cooling | CERN $\bar{p}$ | Ind Linac |
| :--- | :--- | :---: | :---: | :---: |
| $\int B d \ell$ | Tm | .30 | .088 |  |
| L | m | 1.0 | $\approx 5$ | 5.0 |
| $t_{\text {rise }}$ | ns | $\mathbf{5 0}$ | $\mathbf{9 0}$ | $\mathbf{4 0}$ |
| B | T | . $\mathbf{3 0}$ | $\approx \mathbf{0 . 0 1 8}$ | $\mathbf{0 . 6}$ |
| X | m | .42 | .08 |  |
| Y | m | .63 | .25 |  |
| $\mathrm{~V}_{1 \text { turn }}$ | kV | $\mathbf{3 , 9 7 0}$ | $\mathbf{8 0 0}$ | $\mathbf{5 , 0 0 0}$ |
| $\mathrm{U}_{\text {magnetic }}$ | J | $\mathbf{1 0 , 4 5 0}$ | $\approx \mathbf{1 3}$ | $\mathbf{8 0 0 0}$ |

## Note

- U is 3 orders above $\bar{p}$, and 1 order of magnitude more than 30 pi mm FFAG
- Same order as Induction
- And $t$ same order as a few $m$ of induction linac
- But V is too High for single turn kicker


## Induction Kicker

- Drive Flux Return
- Subdivide Flux Return Loops

Solves Voltage Problem

- Conducting Box Removes

Stray Field Return


End View


Side View

## Works with no Ferrite

- $\mathrm{V}=$ the same
- U $\approx 2.25 \times$
- $1 \approx 2.25 \times$
- No rise time limit
- Not effected by solenoid fields


End View


- If non Resonant: 2 Drivers
for inj. \& extract.
Need $24 \times 2$ Magamps ( $\approx 20 \mathrm{M} \$$ )
- If Resonant: 1 Driver, $2 \times$ efficient Need 12 Magamps ( $\approx 5 \mathrm{M} \$$ )


## Magnetic Amplifiers

Used to drive Induction Linacs
similar to ATA or DARHT

3.9 Longitudinal Cooling Conclusion

- Good cooling in 6 D in a ring
- But injection/extraction difficult
- Requires short bunch train
- Good 6D cooling in Gas Helix
- But required very high fields at coils outside RF
- Converting Ring cooler to a large Helix
- Solves Injection/extraction problem
- Solves bunch train length problem
- Allows tapering to improve performance
- But more expensive than ring
- Needs more study


## 4 TUTORIALS

Where to get generic icool files and manual
http://pubweb.bnl.gov/people/fernow/icool/readme.html
Files to Run problems with icool
http://pubweb.bnl.gov/people/palmer/05school/05icool.zip
make a new comand line directory and copy all these files into it.
These files include an icool executable, a basic compiler, a topdraw plotter.
You may later want to use your own compilers and plotters, but this way we can hopefully get instant results.

Try typing any of the following: any one should execute and give a plot on the screen page down should show more plots

- runtrack focus
- runtrack focus0
- runtrack focus1
- runtrack focus2
- runbeta fs2
- runlong cont (but not yet)
- runring ring (nor this yet)


### 4.1 Introduction

All our ICOOL jobs read files: for001.dat (data) and for003.dat (input tracks), and for020.dat (coild desciption) or for045.dat (field description).
They will write for002.dat (a log file) and and for009.dat (an ntuple) among others.
I have short basic programs to read the ntuple and generate top draw plot files: \#\#\#.td which can be converted into tex files for printing.

To keep track of these files when running different jobs, it is convenient to save them with a job name that I will write as \#\#\#. The files are then kept with names:\#\#\#.coi \#\#\#.f01, \#\#\#.f03 etc
4.2 Two Batch Commands: "runtrack", "new"

## Command to Run Program

Type: "runtrack \#\#\#" e.g. "runtrack focus"
this executes the following batch job (runtrack.bat)
copy $\% 1 . f 01$ for001.dat copy main data file
copy $\% 1 . f 03$ for003.dat copy input tracks
copy \%1.coi dirty.dat copy coil definitions
cleaning remove comments after!'s
copy clean.dat coil.dat copy cleaned up coil file
sheet3 Make multiple current sheets for coil blocks
copy sheet.out for020.dat copy sheet data
icool Run ICOOL
TRACK2 Run analysis of ntuple file to make plots copy coil.td + track.td \%1.td Copy plot files
VU \%1.td Vue plots with TOPDRAW

## A Usefull batch command: new \#\#1 \#\#2

copy the "set" of files to a new name prior to making modifications e.g. use: "new focus2 newf1"
names may not be more than 8 characters

```
COPY %1.F01 %2.F01
COPY %1.F03 %2.F03
COPY %1.F45 %2.F45
copy %1.coi %2.coi
```

4.3 Example 1, a very simple case: "focus"

## Main data file: focus.f01

this will be copied to for001.dat main data used by icool

```
Drift space example
! a title
! no of tracks =1
$cont npart=1 
$ints $
$nhs $
$nsc $
$nzh nzhist=0 $ ! no of crude plots vs z
$nrh $
$nem $
$ncv $
SECTION
REPEAT ! repeat till "ENDREPEAT"
150
OUTPUT
! 150 times
! write out data to for009.dat
SREGION ! start an 8 line "region"
0.05 1 0.001 ! deltaz 1 zstep (m)
1 0. 0.10
SOL ! solenoid
! 1 0 rmax
1 0 0 0. 1.8 0. 0. 0. 0. 0. 0.0.0.0.0. ! 1 0 0 0 Bz 0 0 0 0 0 0 0 0 0 0
VAC ! no material, could be CU, BE etc
CBLOCK ! dummy material shape
    0.0.0.0.0. 0.0.0.0.0. ! dummy material shape
ENDREPEAT ! end repeat
ENDSECTION ! end of run
```


## Input tracks file: \#\#\#.f03

\#\#\#.f03 copied to for003.dat initial tracks used by icool this example (focus.f03) has only two tracks. Add one line each for more.

lengths in $m$, momenta in $\mathrm{GeV} / \mathrm{c}, \mathrm{t}$ in seconds. P 's are polarization

## Coil File \#\#\#.coi

In this case the field is defined in the \#\#\#.f01 file so the coil file is ignored

## Log file: FOR002.dat

for002.dat log written by icool which lists of regions, error messages, and crude plots (I do not use these)

## Ntuple output file: FOR009.dat

written by the "OUTPUT" commands in the for001.dat data file
The first line hs a title, the second units, then the track data. e.g.

```
# Drift space example
! title
# units = [s] [m] [GeV/c] [T] [V/m] ! units
i par typ flg reg t x y z Px
```


### 4.4 Example 2: .f01 Example with coil Specified

```
focus1
title
$cont npart=1
number of particles to track
nprnt=3 prlevel=1 bgen=.false. $
$ints $
$nhs $
$nsc $
$nzh nzhist=0 $
$nsc $
$nzh $
$nrh $
$nem $
$ncv $
SECTION
CELL
1
.true.
SHEET
fields from sheets in for020.dat
3 20.0025 .0025 6 0.24 99 1 0 0 0 0 0 0 0 ! mode file dl dr l r reach interp
REPEAT
repeat following regions
120
120 times
OUTPUT
print ntpl here
SREGION
a region has }8\mathrm{ lines
0.05 1 0.001
deltaz 1 zstep
1 0. 0.24
1 0 rmax
NONE
dummy for RF or other field
    0.0.00000000000000
VAC
vacuum
CBLOCK
dummy for shape of material
    0.0.0.0.0. 0.0.0.0.0.
ENDREPEAT
end repeat loop
ENDCELL
end cell
ENDSECTION
end of everything
```


## Coil Definitions \#\#\#.coi

for020. dat coil sheets used by icool is generated by basic prog SHEET3 using coil descriptions
in \#\#\#.coi
e.g. focus2.coi

```
alternating strong sols new
```


which generates the following "for020.dat" format and a topdraw picture in "coil.td"

```
alternating strong sols new
```

61
$\begin{array}{llll}1 & 2 & .5 & .2583333 \\ 600000\end{array}$
$\begin{array}{llll}2 & 2 & .5 & .275 \\ 600000\end{array}$
$\begin{array}{lllll}3 & 2 & .5 & .2916667 & 600000\end{array}$
4 3 . 5 . $255-400000$
$\begin{array}{lllll}5 & 3 & .5 & .265-400000\end{array}$
$\begin{array}{lllll}6 & 3 & .5 & .275 & -400000\end{array}$
in this case 3 sheets for each coil specified in the .coi

### 4.5 An example with material for cooling: "cont"

## " cont.f01"

C1 Continuous cooling
\$cont npart=100 nsections=1 timelim=500. bgen=.false.
varstep=.true. nprnt=1 prlevel=-1 epsstep=1e-4 ntuple=.false.
phasemodel=3 neighbor=.false. dectrk=.true.
fsav=.false. izfile=1160 bunchcut=1. spin=.true. output1=.true.
timelim=9999 \$
\$bmt nbeamtyp=1 \$
13 1. 1 ! 2ndary pion---not used because bgen=false above
$0.0 .00 .179 \quad 0.0000$ !mean: x y z px py pz
0. 0. 0. $0.0 \quad 0.0 \quad 0 . \quad$ !sigs

0
\$ints ldecay=.true. declev=1 !details of scattering and straggling - see manual
ldedx=.true. lstrag=.true. lscatter=.true.
delev=2 straglev=4 scatlev=4 \$
\$nhs \$ !
\$nsc \$ !
\$nzh nzhist=0 \$
no of crude plots vs z
\$nsc \$
!
\$nzh \$
\$nrh \$
!
!
\$nem \$
\$ncv \$
SECTION
REFP
2 . 2 0. $0 \quad 3$
BEGS
CELL
50 ! number of following cells
.true. ! alternating signs of Bz in each cell


```
1 0. 0.18
NONE
    0.0.0.0.0. 0.0.0.0.0.0.0.0.0.0.
LH
CBLOCK
    0.0.0.0.0. 0.0.0.0.0.
SREGION ! Hydrogen window
0.0025 1 2e-3
1 0. 0.5
NONE
    0.0.0.0.0. 0.0.0.0.0. 0.0.0.0.0.
AL
CBLOCK
    0.0.0.0.0. 0.0.0.0.0.
```

```
SREGION ! 1st free
```

SREGION ! 1st free
0.2575 1 2e-3
0.2575 1 2e-3
1 0. 0.5
1 0. 0.5
NONE
NONE
0.0.0.0.0. 0.0.0.0.0.0.0.0.0.0.
0.0.0.0.0. 0.0.0.0.0.0.0.0.0.0.
vAC
vAC
CBLOCK
CBLOCK
0.0.0.0.0. 0.0.0.0.0.
0.0.0.0.0. 0.0.0.0.0.
REPEAT
3
SREGION !RF
0.470 1 5e-3
1 0. 0.65
ACCEL
2. 201.25 15.48 29.80 0. 0. 0.0.0.0. 0.0.0.0.0.! mode freq
VAC
NONE
0.0.0.0.0. 0.0.0.0.0.

```
ENDR
```

SREGION ! RF 4
0.47 1 5e-3
1 0. 0.65
ACCEL
2. 201.25 15.48 29.80 0. 0. 0.0.0.0. 0.0.0.0.0.
VAC
NONE
0.0.0.0.0. 0.0.0.0.0.

```
\begin{tabular}{lllll} 
SREGION & & & ! free \\
0.2575 & & 1 & \(2 \mathrm{e}-3\) \\
1 & 0. & 0.5 & &
\end{tabular}
NONE
    0.0.0.0.0. 0.0.0.0.0.0.0.0.0.0.
VAC
CBLOCK
    0.0.0.0.0.0.0.0.0.0.
SREGION ! Hydrogen window
\(0.0025 \quad 1 \quad 2 \mathrm{e}-3\)
10.0 .5
NONE
    0.0.0.0.0. 0.0.0.0.0.0.0.0.0.0.
AL
CBLOCK
    0. 0. 0. 0. 0. 0. 0. 0. 0. 0.
OUTPUT
SREGION ! 2nd 1/2 absorber
\(0.175 \quad 1 \quad 3 \mathrm{e}-3\)
10.0 .18
NONE
    0.0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0.
LH
CBLOCK
    0. 0. 0. 0. 0. 0. 0. 0. 0. 0 .
ENDCELL
ENDSECTION
4.6 Description of Jobs
1. runtrack focus fixed field
2. runtrack focus0 Long focus coil
3. runtrack focus1 single short focus coil
4. runtrack focus2 two focus coils
5. runbeta fs 2 get betas vs mom for Study 2 Lattice
6. runlong cont cool in a long Study 2 lattice
7. (runring ring cool in a ring)

How to run Icool on Linux
Capri, June 18/19 2005
Ulisse Bravar
University of New Hampshire
System requirements
Fortran compiler f77, g77 or whatever
Graphic package: root, paw, excel
Downloads (1)
Download \#\#\#\#.f01, \#\#\#\#.f03, \#\#\#\#.coi
etc. from
http://pubweb.bnl.gov/people/palmer/04
school/icool2/
dos2unix \#\#\#\#.f01, \#\#\#\#.f03, \#\#\#\#.coi
etc.
E.g. http://www.iconv.com/dos2unix.htm

Copy \#\#\#\#.f01 -i for001.dat etc. Downloads (2)
Download Icool source files i\#\#\#.for and
icommon.inc from
http://pubweb.bnl.gov/people/fernow/ico
ol/v268/
Edit icool.for, disable calls to IN_KEY and CHECK_KEY
g77 icool.for idiag.for imath.for ifld.for
iint.for iunix.f -o icool

Downloads (3)
Download endof9.for ecalc9f.for and ecalc9f.inp from same web page.
Compile endof9 and ecalc9f
Download and compile convert.for endof9.for ecalc9f.for write.c examples and this note from http://wwwpnp.
physics.ox.ac.uk/ bravar/Capri
Also available on stick.
Create current sheets
Copy \#\#\#\#.coi -i coil.coi
Run convert.for
Output file \(=\) for020.dat
This routine takes care of cleaning and sheet3
Simulation and Analysis
Run icool
The main output file is for009.dat
Run endof9
Copy endof9.dat -i for009.dat
Run ecalc9f
Final data file: ecalc9f.dat
Making plots
Edit ecalc9f.dat, read header and then
remove
E.g. plot beta-perp as a function of \(z\) :
a) in paw: \(v /\) read \(a, z, a, a, a, a, a, a, b e t a\)
\(\mathrm{v} /\) plot beta
b) in root: .x write.c
betaperp. Draw(beta:z,,L)
4.7 Excercise 1
1. Run the focus examples by typing:
- "runtrack focus" fixed field
- "runtrack focus0" Long focus coil
- "runtrack focus1" single short focus coil
- "runtrack focus2" two focus coils
2. make a new file called test1 from "focus1" using "new". Modify the new file to explore sensitivity to initial angles.
in test1.f01: Note the max radius in the region command and in the sheet command that sets up the field grid.
3. In test1.coi: Move the start of the coil to 0.5 m (instead of 3 m )
4. In test1.coi: Increase the current so the beam is foucused near the end of \(z\)
5. In test1.f03: Add further tracks with increased initial pt till the tracks pass outside the radius limits.

Do they all focus to the same point?
What is the name for this abberation?
Is it positive or negative?
4.8 Excercise 2: Determine betas of a lattice
1. type "runbeta fs 2 "
2. using "new": make a new file from "fs2" called "beta1".

Then In beta1.coi::
a) Increase the two "focus" coil currents by approx \(20 \%\) which will give smaller betas
b) while decreasing the single "coupling" coil current to obtain betas more or less centered on \(0.2 \mathrm{GeV} / \mathrm{c}\)

How much was the center beta reduced?
Is the momentum acceptance the same?
3. Repeat the above calling it "beta2" with the two "focus" coils currents from fs2 by approx 40\%
4. Repeat the above calling it "beta3" with the two "focus" coils currents from fs2 by exactly 66\%
what is special about \(66 \%\) ?
4.9 Excercise 3: Cooling in a long lattice
1. run "runlong cont"
2. increase the number of particles to 1000 (on line 3 of cont.f01) and run when you have the time to wait.
3. Make a new file set and then substitute a .coi from the previous excersise that had a smaller beta.

Is the final emittance smaller?
Is the acceptance worse?
4. make new file from "cont" called "LiH".
replace hydrogen with \(\mathrm{LiH}(\mathrm{LIH})\) with thickness such as to give same energy loss as H 2 (there is a table of \(\mathrm{dE} / \mathrm{dx}\) in the lecture notes). Replace the Al window with Berilium ( BE ) and run "runlong LiH" with npart=1000.```


[^0]:    ${ }^{1}$ http://www.fnal.gov/projects/muon_collider/FridayMeetings/May\% $2013 \% 2 \mathrm{C} \% 202005 /$ Simulations\% 20 of\% 20 parametric\% 20 Resonance\%20Cooling\% $20-\% 20 B e a r d . p d f ~$

[^1]:    ${ }^{2}$ e.g. s y Lee "Accelerator Physics", eq 3.27
    ${ }^{3}$ e.g. s y Lee "Accelerator Physics", eq 3.55

[^2]:    ${ }^{4}$ MUC-232 \& 246
    ${ }^{5}$ Snowmass Proc.
    ${ }^{6} \mathrm{MUC}-239$
    ${ }^{7} \mathrm{MUC}-146,147,185,187,193,284$

[^3]:    ${ }^{8}$ MUC 185 and 284

[^4]:    ${ }^{9}$ Fernow and others: MUC-232, 265, 268, \& 273
    ${ }^{10}$ V.Balbekov "Simulation of RFOFO Ring Cooler with Tilted Solenoids" MUC-CONF-0264

